## SIDDHARTH INSTITUTE OF ENGINEERING \& TECHNOLOGY:: PUTTUR (AUTONOMOUS)

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## OUESTION BANK (DESCRIPTIVE)

Subject with Code: Mechanics of Solids (20CE0164)
Course \& Branch: B.Tech (ME \& AGE)
Year \& Sem: II \& I
Regulation: R20

## UNIT I

(Simple Stresses and Strains, Theories of failure)

| 1 | a) Define stress and strain. Explain different types of stresses and strains. | L1 | CO1 | 6M |
| :---: | :---: | :---: | :---: | :---: |
|  | b) Draw and explain Stress-strain curve for a mild steel bar. | L1 | CO1 | 6M |
| 2 | a) State Hooke's law with equation. | L1 | CO1 | 2M |
|  | b) A tensile test was conducted on a mild steel bar. The following data was obtained from the test: <br> (i) Diameter of the steel bar $=3 \mathrm{~cm}$ <br> (ii) Gauge length of the bar $=20 \mathrm{~cm}$ <br> (iii) Load at elastic limit $=250 \mathrm{KN}$ <br> (iv) Extension at a load of $150 \mathrm{KN}=0.21 \mathrm{~mm}$ <br> (v) Maximum load $=380 \mathrm{KN}$ <br> (vi) Total extension $=60 \mathrm{~mm}$ <br> (vii) Diameter of the rod at the failure $=2.25 \mathrm{~cm}$. <br> Determine: <br> (a) The Young's modulus, <br> (b) The stress at elastic limit, <br> (c) The percentage elongation, and <br> (d) The percentage decrease in area. | L3 | CO1 | 10M |
| 3 | A brass bar, having cross-sectional area of $1000 \mathrm{~mm}^{2}$, is subjected to axial forces as shown in figure. Find the total elongation of the bar. Take $\mathrm{E}=1.05 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$. | L3 | CO1 | 12M |


| 4 | Two brass rods and one steel rod together support a load as shown in fig. If <br> the stresses in brass and steel are not to exceed $60 \mathrm{~N} / \mathrm{mm}^{2}$ and $120 \mathrm{~N} / \mathrm{mm}^{2}$, <br> find the safe load that can be supported. Take E for steel $=2 \mathrm{~L} 105 \mathrm{~N} / \mathrm{mm}^{2}$ and <br> for brass $=1 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$. The cross-sectional area of steel rod is $1500 \mathrm{~mm}^{2}$ <br> and of each brass rod is $1000 \mathrm{~mm}^{2}$ | CO1 | 12M |
| :--- | :--- | :--- | :--- | :--- |


| $\mathbf{9}$ | The load on the screw consists of an axial pull of 10 kN together with the <br> transverse shear force of 5 kN . Find the diameter of the bolt required according <br> to (i) Maximum principal stress theory. (ii) Maximum principal strain theory. <br> Take Permissible tensile stress at elastic limit $=100 \mathrm{MPa}$ and and Poisson's <br> ratio $=0.3$, factor of safety $=1$. | CO1 | 12 M |
| :--- | :--- | :--- | :--- | :--- |
| $\mathbf{1 0}$ | Determine the diameter of a bolt which is subjected to an axial pull of 9 KN <br> together with a transverse shear force of 4.5 KN using : <br> (i) Maximum shear stress theory. (ii) Maximum strain energy theory. <br> Given the elastic limit in tension $=225 \mathrm{~N} / \mathrm{mm}^{2}$, factor of safety $=3$ and <br> Poisson's ratio $=0.3$. | CO1 | 12 M |

## UNIT II

(Shear Force and Bending Moments, Theory of Simple Bending)

| 1 | A cantilever beam of length 3 m carries a uniformly distributed load of $1.5 \mathrm{kN} / \mathrm{m}$ run over a length of 2 m from the free end. Draw SFD and BMD for the beam. | L3 | CO 2 | 12M |
| :---: | :---: | :---: | :---: | :---: |
| 2 | Draw the shear force and bending moment diagram for a simply supported beam of length 9 m and carrying a uniformly distributed load of $10 \mathrm{kN} / \mathrm{m}$ for a distance of 6 m from the left end. Also calculate the maximum bending moment in the section. | L3 | CO 2 | 12M |
| 3 | A cantilever beam of length 2 m carries the point loads as shown in Fig. Draw the SFD and BMD for the given beam. | L3 | CO 2 | 12M |
| 4 | Draw the shear force and bending moment diagram for overhanging beam carrying uniformly distributed load of $2 \mathrm{kN} / \mathrm{m}$ over the entire length and a point load of 2 kN as shown in Figure. | L3 | CO 2 | 12M |


| $\mathbf{5}$ | A simply supported beam oflength10m carries the UDL and two-point loads as <br> shown in fig. Draw S.F. and B.M. diagram for the beam shown in figure. Also <br> calculate the maximum bending moment. | CO2 | 12M |
| :--- | :--- | :--- | :--- | :--- |
| $\mathbf{6}$ |  |  |  |



## UNIT III

(Shear Stress Distribution, Torsion of Circular Shafts and Springs)

| 1 | Derive shear stress distribution formula for rectangular section with a neat sketch. | L1 | CO3 | 12M |
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| 2 | A timber beam of rectangular section is simply supported at the ends and carries a point load at the centre of the beam. The maximum bending stress is $12 \mathrm{~N} / \mathrm{mm}^{2}$ and maximum shearing stress is $1 \mathrm{~N} / \mathrm{mm}^{2}$, find the ratio of the span to the depth. | L3 | CO3 | 12M |
| 3 | a) Draw the shear stress distribution across: <br> (i) Rectangular section. <br> (ii) Triangular section. <br> (iii) Circular section. <br> (iv) I \& T Sections | L2 | CO3 | 6M |
|  | b) An I-section beam $350 \mathrm{~mm} \times 150 \mathrm{~mm}$ has a web thickness of 10 mm and a flange thickness of 20 mm . If the shear force acting on the section is 40 KN , find the maximum shear stress developed in the I-section. | L3 | CO3 | 6M |
| 4 | Derive shear stress distribution formula for circular section with a neat sketch. | L1 | CO3 | 12M |


| $\mathbf{5}$ | The shear force acting on a section of a beam is 50 KN . The section of the beam <br> is of T-shaped of dimensions 100 mm x 100 mm x 20 mm as shown in figure. <br> The moment of inertia about the horizontal neutral axis is $314.221 \times 10^{4} \mathrm{~mm}^{4}$. <br> Calculate the shear stress at the neutral axis and at the junction of the web and <br> the flange. | CO3 | 12M |
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## UNIT IV

(Deflection of Beams and Columns)

| 1 | Derive the relation between slope, deflection and radius of curvature. | L2 | CO4 | 12M |
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| 2 | A beam of uniform rectangular section 200 mm wide and 300 mm deep is simply supported at its ends. It carries a uniformly distributed load of 9 $\mathrm{KN} / \mathrm{m}$ run over the entire span of 5 m . If the value of E for the beam material is $1 \times 10^{4} \mathrm{~N} / \mathrm{mm}^{2}$, find: <br> (i) The slope at the supports and (ii) Maximum deflection. | L3 | CO4 | 12M |
| 3 | Determine: (i) slope at the left support, (ii) deflection under the load and (iii) maximum deflection of a simply supported beam of length 5 m , which is carrying a point load of 5 KN at a distance of 3 m from the left end. Take E $=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ and $\mathrm{I}=1 \times 10^{8} \mathrm{~mm}^{4}$. | L3 | CO4 | 12M |
| 4 | A cantilever of length 3 in carries two-point loads of 2 KN at the free end and 4 KN at a distance of 1 m from the free end. Find the deflection at the free end. Take $\mathrm{E}=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ and $\mathrm{I}=10^{8} \mathrm{~mm}^{4}$ | L3 | CO4 | 12M |
| 5 | A horizontal beam AB is simply supported at A and $\mathrm{B}, 6 \mathrm{~m}$ apart. The beam is subjected to a clockwise couple of $300 \mathrm{KN}-\mathrm{m}$ at a distance of 4 m from the left end as shown in figure below if $\mathrm{E}=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ and $\mathrm{I}=2 \times 10^{8}$ $\mathrm{mm}^{4}$, determine: <br> (i) Deflection at the point where couple is acting and <br> (ii) The maximum deflection. | L3 | CO4 | 12M |
| 6 | a) Write the assumptions made in the Euler's column theory. | L2 | CO5 | 4M |
|  | b) Write the end conditions for long columns and state the difference between long columns and short columns. | L2 | CO5 | 8M |
| 7 | Derive an expression for crippling load when both ends of the column are hinged. | L2 | CO5 | 12M |


| $\mathbf{8}$ | A solid round bar 3 m long and 5 cm in diameter is used as a strut with both <br> ends hinged. (Take $\mathrm{E}=2.0 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ ). Determine the crippling load, <br> when the given strut is used with the following conditions: <br> (i) $\quad$ One end of the strut is fixed and the other end is free <br> (ii) $\quad$ Both the ends of strut are fixed <br> (iii) $\quad$ One end is fixed and other is hinged. | CO5 | 12M |  |
| :---: | :--- | :--- | :--- | :--- |
| $\mathbf{9}$ | A column of timber section 15 cm x 20 cm is 6 metre long both ends being <br> fixed. If the Young's modulus for timber $=17.5 \mathrm{KN} / \mathrm{mm}^{2}$, determine: <br> (i) $\quad$Crippling load and <br> (ii) $\quad$ Safe load for the column if factor of safety $=3$. | L3 | CO5 | 12 M |
| $\mathbf{1 0}$ | Using Euler's formula, calculate the critical stresses for a series of struts <br> having slenderness ratio of $40,80,120,160$ and 200 under the following <br> conditions: <br> (i) Both ends hinged and <br> (ii) Both ends fixed. Take $\mathrm{E}=2.05 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ | CO5 | 12 M |  |

## UNIT V

(Thin Cylinders and Thick Cylinders)

| 1 | a) Derive expression for circumferential stress in thin cylinder. | L2 | CO6 | 6M |
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|  | b) A cylindrical pipe of diameter 1.5 m and thickness 1.5 cm is subjected to an internal fluid pressure of $1.2 \mathrm{~N} / \mathrm{mm}^{2}$. Determine: <br> (i) Longitudinal stress developed in the pipe, and <br> ii) Circumferential stress developed in the pipe. | L3 | CO6 | 6M |
| 2 | A cylindrical thin drum 80 cm in diameter and 3 m long has a shell thickness of 1 cm . If the drum is subjected to an internal pressure of $2.5 \mathrm{~N} / \mathrm{mm}^{2}$, Take $\mathrm{E}=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ and Poisson's ratio 0.25 <br> Determine <br> (i) change in diameter <br> (ii) change in length and <br> (iii) Change in volume. | L3 | CO6 | 12M |
| 3 | A cylindrical shell 100 mm long 200 mm internal diameter having thickness of a metal as 10 mm is filled with a fluid at atmospheric pressure. If an additional $200 \mathrm{~mm}^{3}$ pumped into the cylinder, Take $\mathrm{E}=2 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ and Poisson's ratio is 0.3 . Find <br> (i) The pressure exerted by the fluid on the cylinder and <br> (ii) The hoop stress induced. | L3 | CO6 | 12M |
| 4 | A copper cylinder, 90 cm long, 40 cm external diameter and wall thickness 6 mm has its both ends closed by rigid blank flanges. It is initially full of oil at atmospheric pressure. Calculate additional volume of oil which must be pumped into it in order to raise the oil pressure to $5 \mathrm{~N} / \mathrm{mm}^{2}$ above atmospheric pressure. For copper assume $\mathrm{E}=1.0 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ and Poisson's ratio $1 / 3$. Take bulk modulus of oil as $\mathrm{K}=2.6 \times 10^{3} \mathrm{~N} / \mathrm{mm}^{2}$. | L3 | CO6 | 12M |
| 5 | A closed cylindrical vessel made of steel plates 4 mm thick with plane and, carries fluid under a pressure of $3 \mathrm{~N} / \mathrm{mm}^{2}$. The dia. of cylinder is 30 cm and length is 80 cm , calculate the longitudinal and hoop stresses in the cylinder wall and determine the change in diameter, length and volume of the cylinder. Take $\mathrm{E}=2 \times 10{ }^{5} \mathrm{~N} / \mathrm{mm}^{2}$ and Poisson's ratio is 0.286 | L3 | CO6 | 12M |
| 6 | a) A cylinder of thickness 1.5 cm has to withstand maximum internal pressure of $1.5 \mathrm{~N} / \mathrm{mm}^{2}$. If the ultimate tensile stress in the material of the cylinder is $300 \mathrm{~N} / \mathrm{mm}^{2}$, factor of safety 3.0 and joint efficiency $80 \%$, determine the diameter of the cylinder. | L3 | CO6 | 6M |


|  | b) A spherical shell of internal diameter 0.9 m and of thickness 10 mm is subjected to an internal pressure of $1.4 \mathrm{~N} / \mathrm{mm}^{2}$. Determine the increase in diameter and increase in volume. Take $\mathrm{E}=2 \mathrm{X} 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$ and $\mu=1 / 3$. | L3 | CO6 | 6M |
| :---: | :---: | :---: | :---: | :---: |
| 7 | Derive an expression for hoop and radial stresses across thickness of the thick cylinder. | L2 | CO6 | 12M |
| 8 | Determine the maximum and minimum hoop stress across the section of a pipe of 400 mm internal diameter and 100 mm thick, when the pipe contains a fluid at a pressure of $8 \mathrm{~N} / \mathrm{mm}^{2}$. Also sketch the radial pressure and hoop stress distribution across the section. | L3 | CO6 | 12M |
| 9 | A compound cylinder is made by shrinking a cylinder of external diameter 300 mm and internal diameter of 250 mm over another cylinder of external diameter 250 mm and internal diameter 200 mm . The radial pressure at the junction after shrinking is $8 \mathrm{~N} / \mathrm{mm}^{2}$. Find the final stresses set up across the section, when the compound cylinder is subjected to an internal fluid pressure of $84.5 \mathrm{~N} / \mathrm{mm}^{2}$. | L3 | CO6 | 12M |
| 10 | A steel cylinder of 300 mm external diameter is to be shrunk to another steel cylinder of 150 mm internal diameter. After shrinking, the diameter at the junction is 250 mm and radial pressure at the common junction is 28 $\mathrm{N} / \mathrm{mm}^{2}$. Find the original difference in radii at the junction. Take $\mathrm{E}=2 \mathrm{x}$ $10^{5} \mathrm{~N} / \mathrm{mm}^{2}$. | L3 | CO6 | 12M |

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